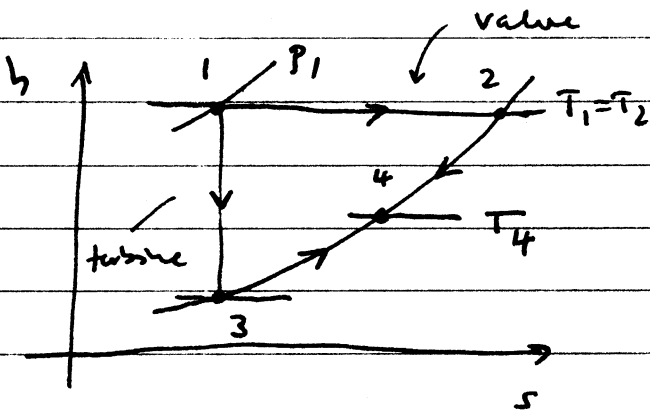


- Assume:
- adiabatic, ideal turbine
 - steady-state
 - ideal gas, const. spec. heats
 - neglect $\Delta KE, \Delta PE$



Note: $P_3 = P_2 = P_4$ mixing at const. pressure
 1st law nozzle: $h_1 = h_2$ (lost work!)

find: \dot{m}_T, \dot{W}_T

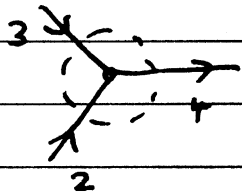
- ad. rev. expansion through turbine:

$$T_3 = T_1 \left(\frac{P_3}{P_1} \right)^{\frac{\gamma-1}{\gamma}} \quad T_2 = 470.7 \text{ K}$$

- Nozzle: $T_2 = T_1 = 644.3 \text{ K}$ (1st law)

- cons of mass: $\dot{m}_T + \dot{m}_V = \dot{m}$

- 1st law CV:

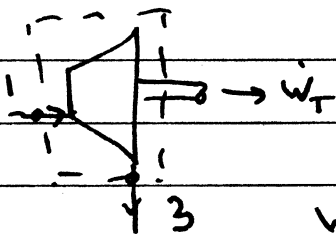


$$0 = \dot{m}_T h_3 + \dot{m}_V h_2 - \dot{m} h_4$$

$$\dot{m}_T = \dot{m} \frac{h_2 - h_4}{h_2 - h_3} = \dot{m} \frac{T_2 - T_4}{T_2 - T_3}$$

$\dot{m}_T = 7.26 \text{ kg/s}$

- 1st law CV



$$0 = -\dot{W}_T + \dot{m}_T (h_1 - h_3)$$

$$\dot{W}_T = \dot{m}_T c_p (T_1 - T_3) ; \quad \dot{W}_T = 1.26 \text{ MW}$$

T2

16. Uniped Spring 2008

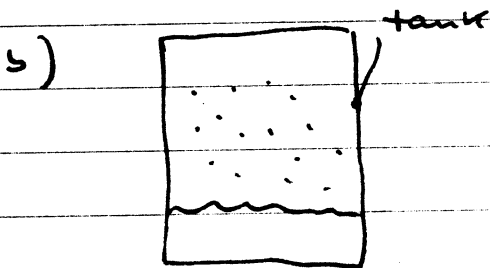
Concepts: 2 phase media, def. of quality

$$a) \quad \bar{v} = v_g(T)x + (1-x)v_f(T)$$

$$x = 10\% \quad , \quad v_f(T=100^\circ\text{C}) = 0.001044 \text{ m}^3/\text{kg}$$

$$v_g(T=100^\circ\text{C}) = 1.6729 \text{ m}^3/\text{kg}$$

$$\bar{v} = 0.16823 \text{ m}^3/\text{kg}$$



$$V = 2 \text{ m}^3$$

$$V_f = 0.5 \text{ m}^3$$

$$\text{so } V_g = 1.5 \text{ m}^3$$

$$P_g = P_f = p = 50 \text{ kPa}$$

$$\hookrightarrow v_f = 0.00103 \text{ m}^3/\text{kg}$$

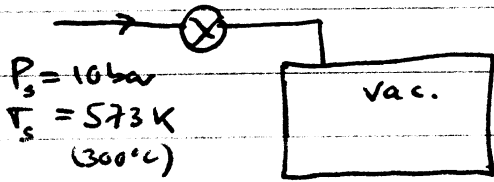
$$v_g = 3.24 \text{ m}^3/\text{kg}$$

$$\text{so } m_f = \frac{V_f}{v_f} = 485.44 \text{ kg} \quad , \quad m_g = \frac{V_g}{v_g} = 0.463 \text{ kg}$$

$$\text{hence } m = m_f + m_g \quad , \quad x = \frac{m_g}{m}$$

$$\underline{x = 0.095\%}$$

$$\underline{m = 485.9 \text{ kg}}$$



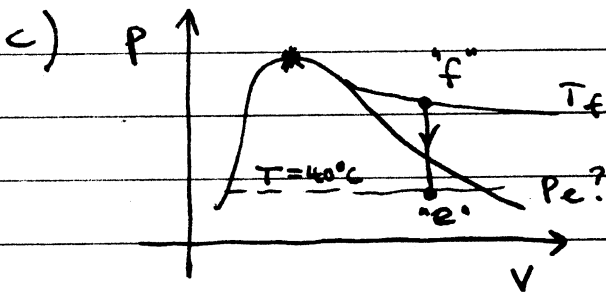
Concepts: - 1st law
 - flow work / enthalpy
 - 2 phase media

a) 1st law CM: $u_f - u_i = -(-P_s v_s)$ flow work done on steam
 CM \rightarrow 1 kg of steam initially: $u_i = u_s$

(insulated valve $\rightarrow q=0$)
 $u_f = u_s + P_s v_s \rightarrow u_f = h_s$

$h_s(P_s, T_s) = 3051.2 \text{ kJ/kg}$, $u_f(T_f) = h_s \rightarrow T_f = 456.2^\circ\text{C}$
 (page 7) \uparrow (table p. 7) interpolate

b) because flow work was done on the steam (see a))



steam cooled (condensing) at constant volume (valve closed, same amount of steam $\rightarrow v = \text{const}$)

find $P(T=40^\circ\text{C})$ on vapor-pressure curve

$P_e = 7.384 \text{ kPa}$

d) 1st law:

$du = dq - p dv \rightarrow 0$ $u_i - u_f'' = q$ $u_f'' = 3051.2 \text{ kJ/kg}$

find v_f'' from table p. 7 $v_f'' = 0.3333 \text{ m}^3/\text{kg}$

$v_f'' = v_i = v_g(40^\circ\text{C})x + (1-x)v_f(40^\circ\text{C})$ $x = \frac{v_f'' - v_f(40^\circ\text{C})}{v_g(40^\circ\text{C}) - v_f(40^\circ\text{C})} = 0.017$

$u_i = u_g(40^\circ\text{C})x + (1-x)u_f(40^\circ\text{C}) = 206.1 \text{ kJ/kg}$

$q = u_i - u_f''$; $q = -2845.1 \text{ kJ/kg}$ heat rejected